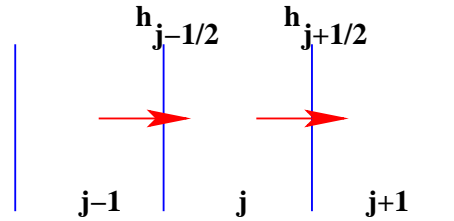


ARTIFICIAL DIFFUSION AND UPWINDING FOR SYSTEMS OF CONSERVATION LAWS

Antony Jameson
Department of Aeronautics and Astronautics
Stanford University, Stanford, CA

☞ UPWIND BIASING FOR A SYSTEM AND FLUX DIFFERENCE SPLITTING



Suppose that a **system of conservation laws**

$$\frac{\partial w}{\partial t} + \frac{\partial}{\partial x} f(w) = 0$$

is approximated by the **semi-discrete scheme**

$$\Delta x \frac{dw_j}{dt} + h_{j+\frac{1}{2}} - h_{j-\frac{1}{2}} = 0$$

where the **numerical flux** is

$$h_{j+\frac{1}{2}} = \frac{1}{2} (f_{j+1} + f_j) - d_{j+\frac{1}{2}}$$

and $d_{j+\frac{1}{2}}$ is a **diffusive flux**. Represent the mean value

Jacobian matrix $A(w) = \frac{\partial f}{\partial w}$ by $A_{j+\frac{1}{2}}$ such that

$$A_{j+\frac{1}{2}} (w_{j+1} - w_j) = f_{j+1} - f_j$$

following the definition of Roe. Set

$$A_{j+\frac{1}{2}} = T \Lambda T^{-1}$$

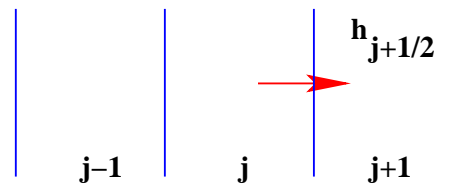
where the eigenvectors of A are columns of T and Λ contains the eigenvalues. Now set

$$d_{j+\frac{1}{2}} = \frac{1}{2} |A_{j+\frac{1}{2}}| (w_{j+1} - w_j)$$

where

$$|A_{j+\frac{1}{2}}| = T |\Lambda| T^{-1}$$

☞ GENERAL MODEL FOR NUMERICAL FLUX AND ARTIFICIAL DIFFUSION



The numerical flux is

$$h_{j+\frac{1}{2}} = \frac{1}{2} (f_{j+1} + f_j) - d_{j+\frac{1}{2}}$$

Introduce [Roe's](#) linearization

$$f_{j+1} - f_j = A_{j+\frac{1}{2}} (w_{j+1} - w_j)$$

Define the [diffusive flux](#) as

$$d_{j+\frac{1}{2}} = \frac{1}{2} B_{j+\frac{1}{2}} (w_{j+1} - w_j)$$

where B is a function of A .

Expand B as a [power series](#)

$$B = \alpha_0 I + \alpha_1 A + \alpha_2 A^2$$

where higher powers are eliminated by the [Cayley Hamilton theorem](#) .

☞ GENERAL MODEL FOR NUMERICAL FLUX AND ARTIFICIAL DIFFUSION (continued)

Three main classes of schemes can thus be identified depending on the number of terms in the expansion

1 term : scalar diffusion

$$d_{j+\frac{1}{2}} = \alpha_0 \Delta w_{j+\frac{1}{2}}$$

2 terms : CUSP, HLL, AUSM

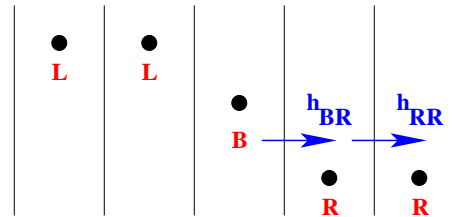
$$\begin{aligned} d_{j+\frac{1}{2}} &= (\alpha_0 I + \alpha_1 A) \Delta w_{j+\frac{1}{2}} \\ &= \alpha_0 \Delta w_{j+\frac{1}{2}} + \alpha_1 \Delta f_{j+\frac{1}{2}} \end{aligned}$$

3 terms : α_0 , α_1 , and α_2 can be chosen so that $B = |A|$ (characteristic splitting) by solving

$$\alpha_0 + \alpha_1 \lambda_k + \alpha_2 \lambda_k^2 = |\lambda_k|, \quad k = 1, 2, 3$$

Criteria for choosing coefficients for these schemes can be based on **positivity** and **numerical shock structure** .

☞ DISCRETE SHOCK STRUCTURE WITH CUSP SCHEMES



The **numerical flux** is defined as

$$h_{j+\frac{1}{2}} = \frac{1}{2} (f_{j+1} + f_j) - d_{j+\frac{1}{2}}$$

where the **diffusive flux** is

$$d_{j+\frac{1}{2}} = \frac{1}{2} \alpha^* c \Delta w_{j+\frac{1}{2}} + \frac{1}{2} \beta \Delta f_{j+\frac{1}{2}}$$

and in **supersonic** flow the scheme is **upwind**

$$\alpha^* = 0 \quad \text{and} \quad \beta = \text{sign}(M) \quad \text{when} \quad |M| \geq 1$$

At the **entrance** to the **shock**

$$h_{LB} = f_L \quad \text{because} \quad M_{LB} > 1$$

maintaining equilibrium. At the **downstream side**

$$\begin{aligned} h_{RR} &= f_R \quad (\text{since } w \text{ and } f \text{ are constant}) \\ h_{BR} &= \frac{1}{2} (f_R + f_B) - \frac{1}{2} \beta (f_R - f_B) - \frac{1}{2} \alpha^* c (w_R - w_B) \end{aligned}$$

Equating these

$$(1 + \beta) (f_R - f_B) + \alpha^* c (w_R - w_B) = 0$$

This is the **Hugoniot** condition for a shock speed $\frac{-\alpha^* c}{1 + \beta}$

☞ DISCRETE SHOCK STRUCTURE WITH CUSP SCHEMES (continued)

Since

$$(f_R - f_B) = A_{BR}(w_R - w_B),$$

this is also an **eigenvalue problem**,

$$A_{BR}(w_R - w_B) + \frac{\alpha^* c}{1 + \beta}(w_R - w_B) = 0$$

For a solution $\frac{-\alpha^* c}{1 + \beta}$ must be an eigenvalue of A_{BR} .

When $u > 0$ the only negative eigenvalue is $u - c$.

Hence

$$\frac{\alpha^* c}{1 + \beta} = c - u$$

giving a **1 parameter family** of solutions where α^* determines β .

👉 E-CUSP SCHEME

(Int J. of CFD, 5, 1998, 1-38)

The **diffusive flux** formed as a combination of differences of the **state** and **flux vectors**

$$d_{j+\frac{1}{2}} = \frac{1}{2}\alpha_{j+\frac{1}{2}}^* c(w_{j+1} - w_j) + \frac{1}{2}\beta_{j+\frac{1}{2}} (f_{j+1} - f_j)$$

Full **upwinding** in **supersonic flow** is obtained by setting

$$\alpha_{j+\frac{1}{2}}^* = 0, \quad \beta_{j+\frac{1}{2}} = \text{sign}(M) \quad \text{when } |M| > 1$$

To support a **stationary discrete shock structure** with a **single interior point** α^* and β cannot be chosen independently.

To satisfy equilibrium at the shock exit

$$\alpha^* = (1 + \beta)(1 - M) \quad \text{when } M > 0$$

The choice $\beta = M$ when $|M| < 1$ corresponds to the **HLL scheme**, which is very diffusive.

☞ E-CUSP SCHEME (continued)

To produce a less diffusive scheme [split](#) the [flux vectors](#) as

$$f = uw + f_p, \quad f_p = \begin{pmatrix} 0 \\ p \\ up \end{pmatrix}$$

Then

$f_{j+1} - f_j = \bar{u}(w_{j+1} - w_j) + \bar{w}(u_{j+1} - u_j) + f_{p_{j+1}} - f_{p_j}$
where \bar{u} and \bar{w} are arithmetic averages.

The [effective coefficient](#) of [convective diffusion](#) is thus

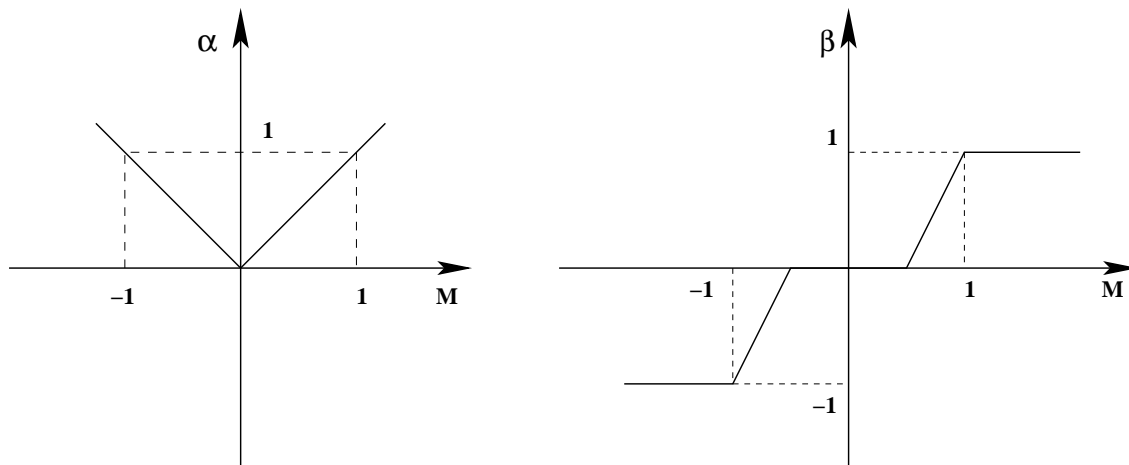
$$\alpha c = \alpha^* c + \beta \bar{u}$$

Take

$$\alpha = |M|$$

Then

$$\beta = \begin{cases} \text{sign}(M) & , \quad |M| \geq 1 \\ \max(2M - 1, 0) & , \quad 0 \leq M \leq 1 \\ \min(2M + 1, 0) & , \quad -1 \leq M \leq 0 \end{cases}$$



CHARACTERISTIC DECOMPOSITION OF THE E-CUSP SCHEME

The **diffusive flux** is

$$\begin{aligned}d_{j+\frac{1}{2}} &= \frac{1}{2}\alpha^*c\Delta w_{j+\frac{1}{2}} + \frac{1}{2}\beta\Delta f_{j+\frac{1}{2}} \\ &= \frac{1}{2}\left(\alpha^*cI + \beta A_{j+\frac{1}{2}}\right)\Delta w_{j+\frac{1}{2}}\end{aligned}$$

where

$$A_{j+\frac{1}{2}}\Delta w_{j+\frac{1}{2}} = \Delta f_{j+\frac{1}{2}}$$

with the **characteristic decomposition**

$$A_{j+\frac{1}{2}} = R\Lambda R^{-1}, \quad \Lambda = \text{diag}(u, u + c, u - c)$$

Thus

$$d_{j+\frac{1}{2}} = RMR^{-1}, \quad M = \text{diag}(\mu_1c, \mu_2c, \mu_3c)$$

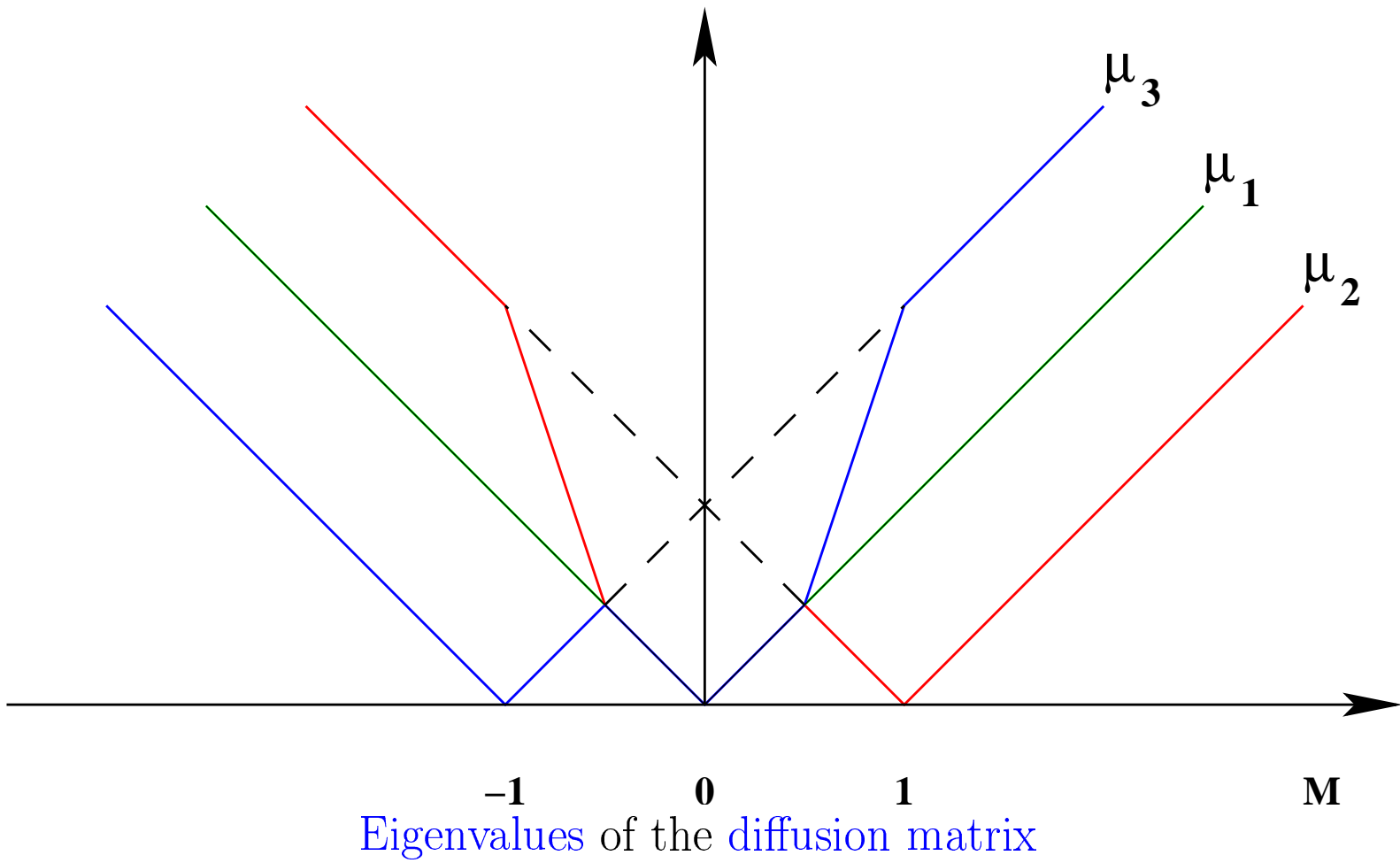
where

$$\begin{aligned}\mu_1 &= \alpha^* + \beta M \\ \mu_2 &= \alpha^* + \beta(M + 1) \\ \mu_3 &= \alpha^* + \beta(M - 1)\end{aligned}$$

Also

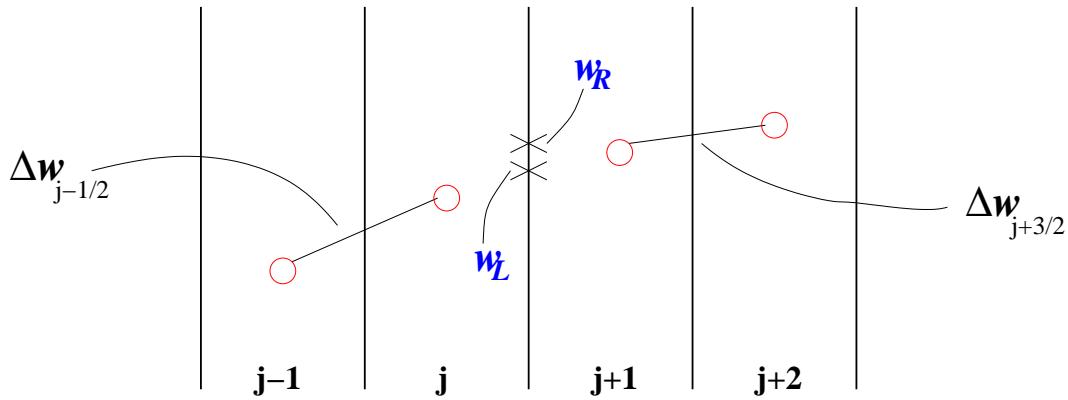
$$\alpha^* = \alpha - \beta M = |M| - \beta M$$

👉 E-CUSP SCHEME



The scheme is **less diffusive** than the **characteristic upwind** scheme.

👉 HIGHER ORDER CUSP SCHEME



Define **left** and **right** states at the interface $j + \frac{1}{2}$

$$w_L = w_j + \frac{1}{2}L \left(\Delta w_{j+\frac{3}{2}}, \Delta w_{j-\frac{1}{2}} \right)$$

$$w_R = w_{j+1} - \frac{1}{2}L \left(\Delta w_{j+\frac{3}{2}}, \Delta w_{j-\frac{1}{2}} \right)$$

$$\text{with } f_L = f(w_L)$$

$$f_R = f(w_R)$$

Then the **numerical flux** is

$$h_{j+\frac{1}{2}} = \frac{1}{2} (f_R + f_L) - \frac{1}{2} \alpha^* c (w_R - w_L) - \frac{1}{2} \beta (f_R - f_L)$$

